

STACKWALL 6'-8"

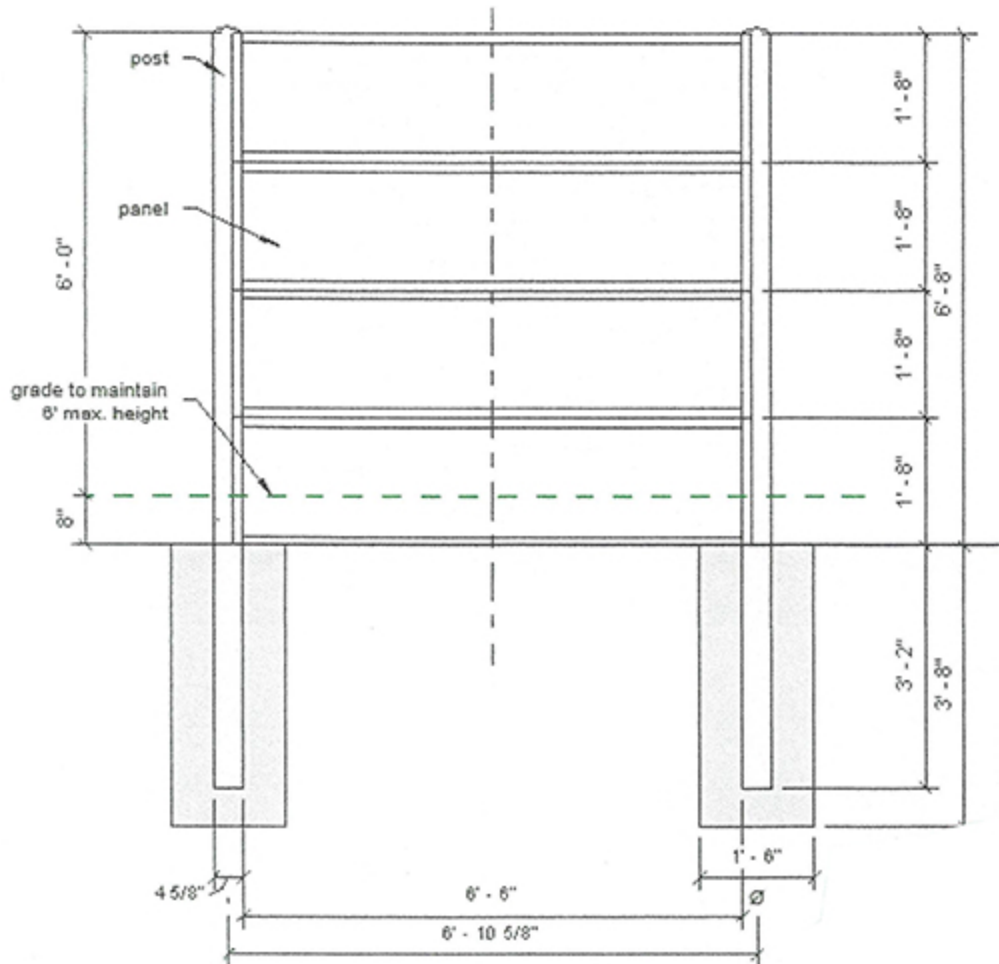
Basic Wall and Site Characteristics

Spacing between posts

$$S_p := 6.88 \cdot ft$$

Wall Height

$$W_h := 6.67 \cdot ft$$



Seismic Design Force

Risk Category 1, Site Class D - Stiff Soil, Seismic Design Category E

$$R := 2.0$$

$$I := 1.0$$

Location

$$\text{Latitude} = 33.99^\circ$$

$$\text{Longitude} = -117.527^\circ$$

Mapped Spectral Response Acceleration Parameters:

$$S_s := 1.591 \cdot g$$

$$S_1 := 0.578 \cdot g$$

Site Coefficients:

$$F_a := 1.2$$

Maximum Considered Earthquake Spectral Response Acceleration Parameters:

$$S_{MS} := S_s \cdot F_a = 1.909 \cdot g$$

Design Spectral Response Acceleration Parameters:

$$S_{DS} := \frac{2}{3} \cdot S_{MS} = 1.273 \cdot g$$

Mapped Long Period Transition:

$$T_L := 8 \cdot \text{sec}$$

Seismic Coefficient

$$C_S := \frac{S_{DS}}{\left(\frac{R}{I}\right)}$$

$$C_S = 0.636 \cdot g$$

Strength

Using ASD

$$V := .7 \cdot C_S$$

$$V = 0.445 \cdot g$$

Panel Thickness $T_p := 2 \cdot \text{in}$ single panel thickness

Panel Weight $W_t := T_p \cdot 150 \cdot \text{pcf}$ $W_t = 25 \text{ psf}$

Seismic Unit Force $v := W_t \cdot \frac{V}{g}$ $v = 11.137 \text{ psf}$

Using Strength $v_s := \frac{W_t \cdot C_s}{g} = 15.91 \text{ psf}$

Wind

Risk Category I, 90 MPH, 3 sec gusts,
Basic Wind Speed Exposure C

$V := 90$ $K_d := .85$ $G := 0.85$ $I := 1.0$ $K_{zt} := 1.0$ $K_z := .85$

$q_z := .00256 \cdot K_z \cdot K_{zt} \cdot K_d \cdot V^2 \cdot \text{psf} = 14.982 \text{ psf}$

$q_s := 0.6 \cdot q_z = 8.989 \text{ psf}$ ASD (16-12)

Design

$q := \text{if}(q_z > v_s, q_z, v_s) = 15.91 \text{ psf}$

Typical Panel Loads

Panel height $h_p := 20 \cdot \text{in}$

Panel length $l_p := 78 \cdot \text{in}$

$w := q \cdot h_p = 26.517 \frac{\text{lbf}}{\text{ft}}$

Moment in Panel

$M_u := \frac{w \cdot l_p^2}{8}$ $M_u = 140.041 \text{ lbf} \cdot \text{ft}$

Panel Reinforcing

$$\phi := .85 \quad f'_c := 4000 \cdot \text{psi} \quad f_y := 40000 \cdot \text{psi} \quad b := 20 \cdot \text{in} \quad d := 1 \cdot \text{in}$$

$$\omega' := \frac{M_u}{\phi \cdot f'_c \cdot b \cdot d^2} = 0.025 \quad \omega := \omega' \cdot (1 - .59 \cdot \omega') = 0.024$$

$$\rho := \omega \cdot \frac{f'_c}{f_y} = 0.002 \quad \rho_{min} := \text{if} \left(\rho > \frac{200 \cdot \text{psi}}{f_y}, \rho, \text{if} \left(\frac{4}{3} \cdot \rho < \frac{200 \cdot \text{psi}}{f_y}, \frac{4}{3} \cdot \rho, \frac{200 \cdot \text{psi}}{f_y} \right) \right) = 0.003$$

Required Reinforcing

$$A_s := \rho_{min} \cdot b \cdot d = 0.065 \text{ in}^2$$

$$A_{pro} := \left(\frac{(.25 \cdot \text{in})^2 \cdot \pi}{4} \right) \cdot 3 = 0.147 \text{ in}^2$$

Use (3) - Ø 1/4" bars horizontal
with Ø 1/4" @ 13" o.c. vertical
Grade 40 bars, $f'_c = 4000$ psi

Post Load

$$M_p := S_p \cdot \frac{W_h^2}{2} \cdot q = (2.435 \cdot 10^3) \text{ lbf} \cdot \text{ft}$$

Post Reinforcing

$$\phi := .85 \quad f'_c := 4000 \cdot \text{psi} \quad f_y := 40000 \cdot \text{psi} \quad b := 4.5 \cdot \text{in} \quad d := 6 \cdot \text{in}$$

$$\omega' := \frac{M_p}{\phi \cdot f'_c \cdot b \cdot d^2} = 0.053 \quad \omega := \omega' \cdot (1 - .59 \cdot \omega') = 0.051$$

$$\rho := \omega \cdot \frac{f'_c}{f_y} = 0.005 \quad \rho_{min} := \text{if} \left(\rho > \frac{200 \cdot \text{psi}}{f_y}, \rho, \text{if} \left(\frac{4}{3} \cdot \rho < \frac{200 \cdot \text{psi}}{f_y}, \frac{4}{3} \cdot \rho, \frac{200 \cdot \text{psi}}{f_y} \right) \right) = 0.005$$

Required reinforcing

$$A_s := \rho_{min} \cdot b \cdot d = 0.139 \text{ in}^2$$

$$A_{pro} := \left(\frac{(.375 \cdot \text{in})^2 \cdot \pi}{4} \right) \cdot 2 = 0.221 \text{ in}^2$$

Use 2-#3 vertical each end
Grade 40 bars, $f'_c = 4000$ psi

Post Shear

$$\rho_w := \rho_{min} = 0.005$$

$$b_p := 1.625 \cdot \text{in}$$

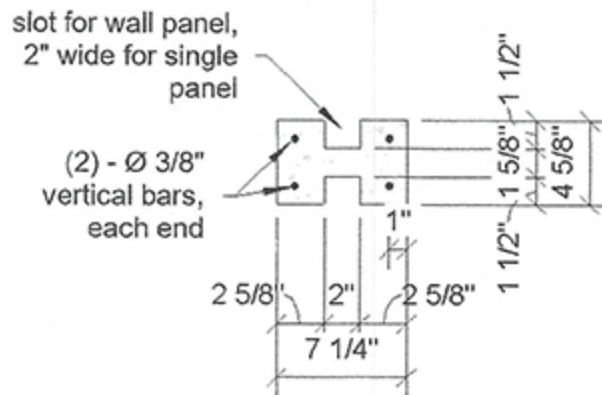
$$d_p := 6.25 \cdot \text{in}$$

$$V_p := S_p \cdot W_h \cdot q = 730.104 \text{ lbf}$$

$$v_p := \frac{V_p}{b_p \cdot d_p} = 71.887 \text{ psi}$$

$$V_c := 2 \cdot \sqrt{(f'_c \cdot \text{psi})} \cdot b_p \cdot d_p$$

$$V_c = (1.285 \cdot 10^3) \text{ lbf}$$



Caisson Depth Required

$$P := q_s \cdot W_h \cdot S_p \cdot \text{if}(q_s > v_s, .6, .7) = 288.753 \text{ lbf}$$

Lateral Bearing Pressure:

$$p := 200 \cdot \frac{\text{psf}}{\text{ft}}$$

Based on Sandy Gravel
CL, ML, MH, CH, Table
1806A.2, including
increase

Diameter of caisson:

$$b := 18 \cdot \text{in}$$

Applied Height

$$h := \frac{W_h}{2}$$

$$h = 3.335 \text{ ft}$$

Assume depth of embedment 44"

$$S_1 := p \cdot \frac{3.67}{3} \cdot \text{ft}$$

$$S_1 = 244.667 \text{ psf}$$

Equation 18-1

$$A := \frac{2.34 \cdot P}{S_1 \cdot b}$$

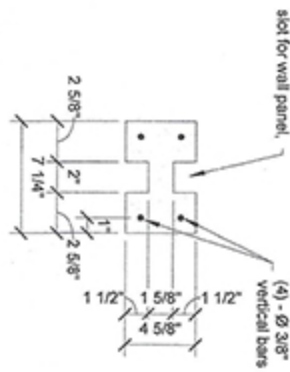
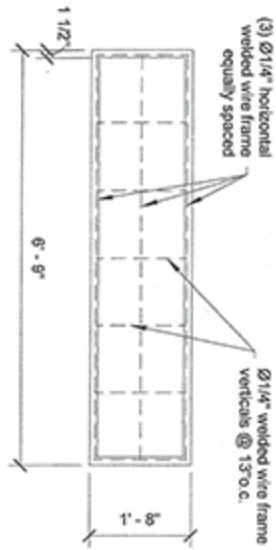
$$A = 1.841 \text{ ft}$$

$$d := 0.5 \cdot A \cdot \left(1 + \left(1 + \left(\frac{4.36 \cdot h}{A} \right)^{\frac{1}{2}} \right) \right)$$

$$d = 3.666 \text{ ft}$$

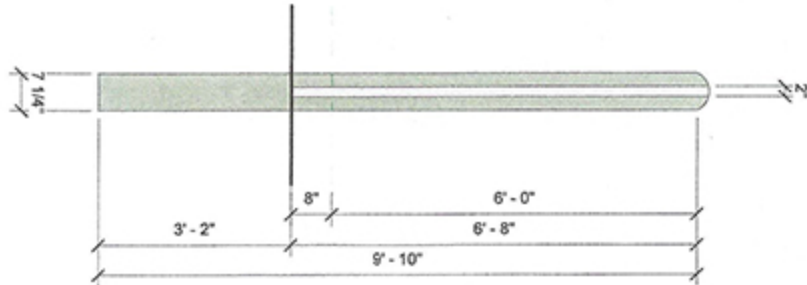
< 44" depth provided

3 Wall Panel
1 1/2" = 1'-0"

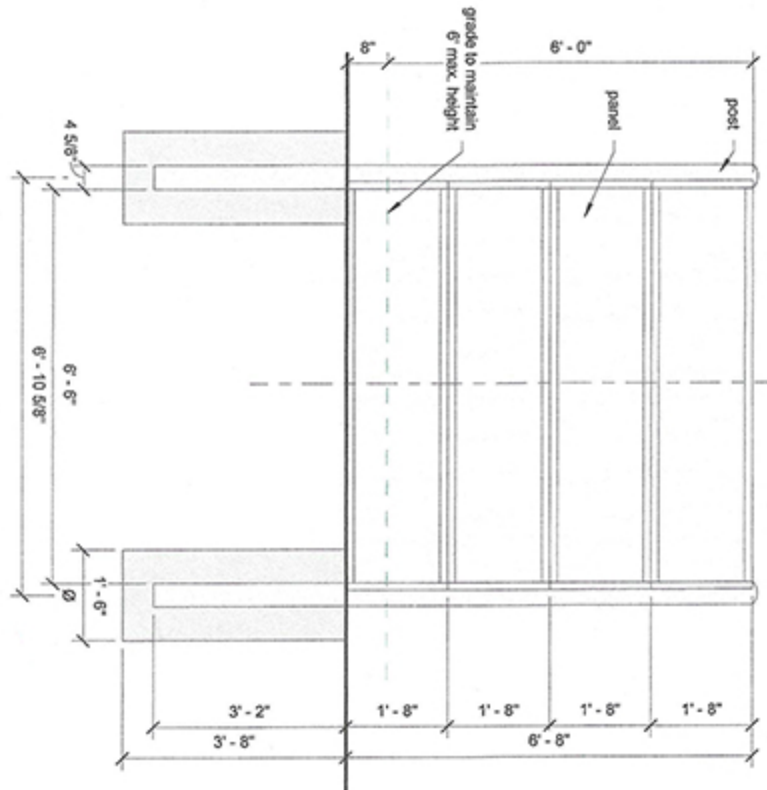


4 Post Section
1 1/2" = 1'-0"

2 Concrete Post
1 1/2" = 1'-0"



1 Elevation
1 1/2" = 1'-0"



STACKWALL

Stackwall 6'-8"

SCALE: As indicated
SHEET: S.1